

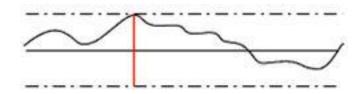


#### **Profile – Tolerance Zones and Evaluation**

• Scope

 Shape Of Zone – Size and location of tolerance zones in Calypso Profile characteristic.

• Evaluation methods for each.





Bilateral - one result

Bilateral with unequal distribution - one result

Unilateral (nominal contour inside)

Unilateral (nominal contour outside)

Bilateral - two results

Bilateral with unequal distribution - two results

Outwards into infinity

Inwards into infinity



## Profile – on-line help



Back Forward Print Option	Shape Of Zone	Will be output:	Example
keyword to find:	Bilateral – one result	Double the largest deviation (inside and outside)	~~~~
ic to display: g the automatic login () g user privileges () pout filtration and outliers ()	Bilateral with unequal distribution – one result	Double the largest deviation (inside and outside) from one of the calculated theoretical center lines	
assword () ristics for Form and Locati ristics for the curve () contour best fit constructio an intersection plane () he Line Profile characterist he Line Profile characterist template (additional featur	Unilateral (nominal contour inside)	Double the largest deviation from the tolerance average to the inside or outside	
template (additional featur template (Circle in Contour template (GDT Profile / GD template (GDT Profile / GD circle in contour best fit ()	Unilateral (nominal contour outside)	Double the largest deviation from the tolerance average to the inside or outside	
Configuration file for user NII file for printout header Jefault name: Internal featu and outlier elimination () s ()	Bilateral – two results	The largest deviation inside (minimum) and the largest deviation outside (maximum) the workpiece	
metry characteristic () d characteristics () et the deviation calculation printout header data for A on of a free form surface on of a plane with a cone ()	Bilateral with unequal distribution – two results	The largest deviation inside (minimum) and the largest deviation outside (maximum) the workpiece	
on of a plane with a cylind users () nents on the CT dataset () g in intersection planes () v of the features ()	Outwards into infinity	The largest deviation inside the workpiece	~~~
ment basics () a CT dataset for measure ements additional feature () ments additional feature () of the results for the curv	Inwards into infinity	The largest deviation outside the workpiece	~~~



#### **Bilateral** Double the largest deviation (inside and outside)

	nner - Free Form Knee Joint	F 11 7 PI		11P 1 5		
The state of the second second second second	sources Fe <u>a</u> tures <u>C</u> onstruction <u>S</u> ize				-Z 🗸	
Select Feature						
💒 🐠 🥍					$\supset 0.5$	
GDT Profile	X				-10.0	
Profile	to Alignment					
	A	Actual	Nominal	Upper Tol.	Lower Tol.	Deviation
Bilateral - one re:	sult Destile to					0.074
Γ	0.500 Profile to	Alignment				0.074
Ĩ	0.000	0.574	0.000	0.5	00	0.574
Feature						
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Primar	Measurement Plan	Operator	 Date		Incremental Pa	ant Numbon
Datum		Master	0.570.774.847.9	r 1, 2009	33	art Mumber
Second	Simulation (Off-Line)					
Datum	Names	Description	Actual	Nominal U	tol Ltol	Dev. Histogr.
Tertiar						
Datum						
	Free Form Surface1	Free Form S	urface	#P (310)		
Actual 0.574	S= 0.134	Min=(8)		ax=(145)	D.287 Form=	0.491
OK R	Best Fit: No Best Fit Profile to Alignment	GDT Prof			0.500	0.574 0.074
	FISTING to Alignment	OPT FIOT				0.0/4



# **Profile – Additional Information (4.10 – 5.0)**

					ZEISS Caly 4.10	pso .00.01	Carl Zei	ss	Date Order	October 30, * order *	2009
	Office Planner - F			and Location <u>P</u> lan CA <u>D</u> Extras	Part Number 27	CMM	Drawing No.		Department: Operator	Master	
∩ 🛱		- 	*		Measurement Pla		* drawingno *		Signature: Profile to Aligni	ment	
Select		Dist	0.202		Free Form Knee		250	0.1	202	in cint <sub>e</sub>	
100000 X 20010	142	X	30.744	30.833	0.200	0.	200		089		1. Second
		Y	2.377	2.425					047		
GD		ż	11.750	11.546					204		
		Dist	0.227	1002-0024	0.250	-0.	250		227		F
	143	Х	30.678	30.777					098		A. 2000
		Y	4.390	4.451				-0.0	061		
		Z	12.256	12.033				0.2	223		
Bila		Dist	0.252		0.250	-0.	250	0.2	252		0.002
	144	X	30.308	30.408				-0.1	100		
		Y	6.354	6.429				-0.0	075		
		Z	12.692	12.455				0.2	237		
		Dist	0.268		0.250	-0.	250	0.2	268		0.018
	145*	Х	30.643	30.755					112		
		Y	8.22.9	8.318					089		
		Z	13.488	13.239					249		
		Dist	0.287		0.250	-0.	250	0.2	287		0.037
Clea	146	Х	32.309	32.437					128		
		Y	6.977	7.054				-0.0			
		Z	13.876	13.647	NUMBER OF STREET	(gar	1000000		229		The Constraint
		Dist	0.273		0.250	-0.	250		273		0.023
	147	Х	32.879	33.013				-0.1			
		Y	5.032	5.099					066		
		Z	13.592	13.366					226		
	_	Dist	0.271		0.250	-0 -13.705 11.769	250 -13.695 11.898	0.2	271	-0.010 -0.129	0.021
				19330	Z Dis1 14 X Y	11.789 -0.153 11.425 -15.701 11.736	11,490 -15,688	0.250	-0.250	-0.153 -0.065 -0.013	
				138h	Z Dist 15 X Y	-0.127 12.099 -17.640	11.844 12.145 -17.627	0.250	-0.250	-0.108 -0.127 -0.046 -0.013	
Actual	ОК	Reset			Z Dist 16 X Y	13.993 -18.223	11.725 14.020 -18.213	0.250	-0.250	-0.082 -0.095 -0.027 -0.010	-1
ОК	Reset				17 X Y	10.823	10.886 13.980 -16.206 10.616	0.250	-0.250	-0.063 -0.069 -0.040 -0.011	-1
			<u> </u>		Z Dist	10.526 -0.100	10.616	0.250	-0.250	-0.091 -0.100	 1/19

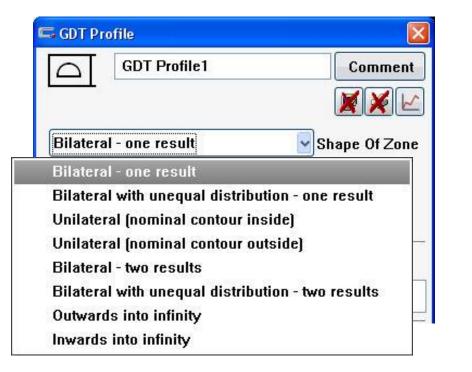


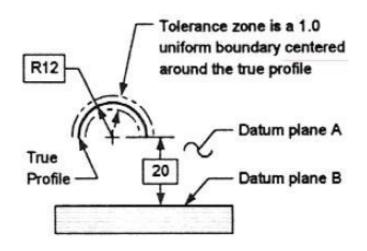
# **Profile – Additional Information (5.2)**

alunno Offico Diann	er - Free Form Knee J	laiat			ZEIS	Calypso 5.2.04		Carl Ze	eiss	Datum Auftrag	7 September 2011 * order *	122
<u>E</u> dit <u>V</u> iew <u>R</u> eso	urces Fe <u>a</u> tures <u>C</u>	onstruction <u>S</u> ize F <u>o</u> rm	and Location Plan CAL	11 mil 11 mil	Teil-Num 42	mer	KMG Prismo	Zeichnungsnumr * drawingno *	mer	Abteilung: Prüfer Unterschrift:	Master	
<b>C</b>	3 🔁 裙 n 🛔			?0	Prüfplan Free For	n Knee Joint				Profile to Align	ment	
ct Fe							Actual	Nominal Upp	er Tolerance Lo	wer Tolerance	Deviation	
	Form Plot Profile to	Alignment			1	X Y Z Dist	11.129 7.799 14.656 -0.063	11.163 7.781 14.707	0.250	-0.250	-0.034 0.018 -0.051 -0.063	-1
7	X	11.050	11.156						-0.106		557	
	Y	-1.475	-1.502						0.027			
	Z	12.175	12.342						-0.167			
	Dist	-0.200	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	0.2	250		-0.250		-0.200			
8/Min	Х	11.043	11.151						-0.108			
Lui l	Y	-3.498	-3.519						0.020			
	Z	11.893	12.065						-0.172			
	Dist	-0.204		0.2	250		-0.250		-0.204			
9	Х	11.037	11.144						-0.107			
	Y	-5.542	-5.556						0.013			
	Z	11.697	11.868						-0.170			1 11
	Dist	-0.202		0.2	250		-0.250		-0.202	2		
					9	Z Dist X	11.893 -0.204 11.037	12.065	0.250	-0.250	-0. 172 -0. 204 -0. 107	-1
144	X	30.308	30.408						-0.100			
	Y	6.354	6.429						-0.075			
	Z	12.692	12.455						0.237			
n <u>e e e e e e e e</u>	Dist	0.268	100 March 100 Ma	0.1	250		-0.250		0.268		0.018	
145/Max	X	30.643	30.755						-0.112		1.000	
	Y	8.229	8.318						-0.089			
	Z	13.488	13.239						0.249		100 C 20 20 20 20 20 20 20 20 20 20 20 20 20	
	Dist	0.287		0.1	250		-0.250		0.287		0.037	
146	X	32.309	32.437						-0.128			
	Y	6.977	7.054						-0.077			
	Z	13.876	13.647	and and					0.229			
	Dist	0.273		0	250	2	-0.250	11.725	0.273		0.023	
ual OK	Reset				16	Dist X Y Z	-0.095 13.993 -18.223 10.823	14.020 -18.213 10.886	0.250	-0.250	-0.095 -0.095 -0.027 -0.010 -0.063	-1
					17	Z Dist X Y	-0.069 13.941	13.980	0.250	-0.250	-0.069	-1
OK Res	et				- CEJ	Z	-16.217 10.526	-16.206 10.616	1998.02	0443025	-0.011 -0.091	22
			11-12-	QQ	1	Dist	-0.100		0.250	-0.250	-0.100	-  1/19

#### **Bilateral – one result** Double the largest deviation (inside and outside)

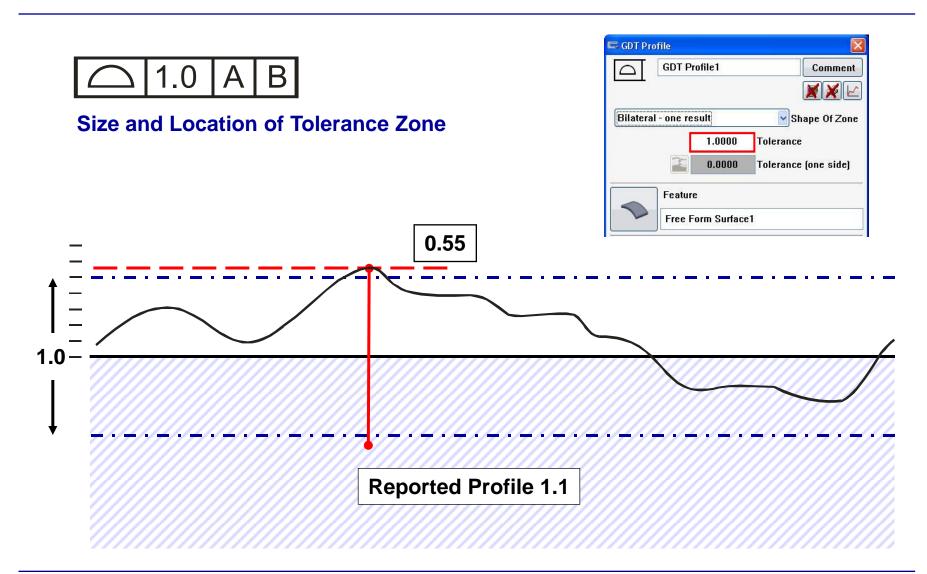






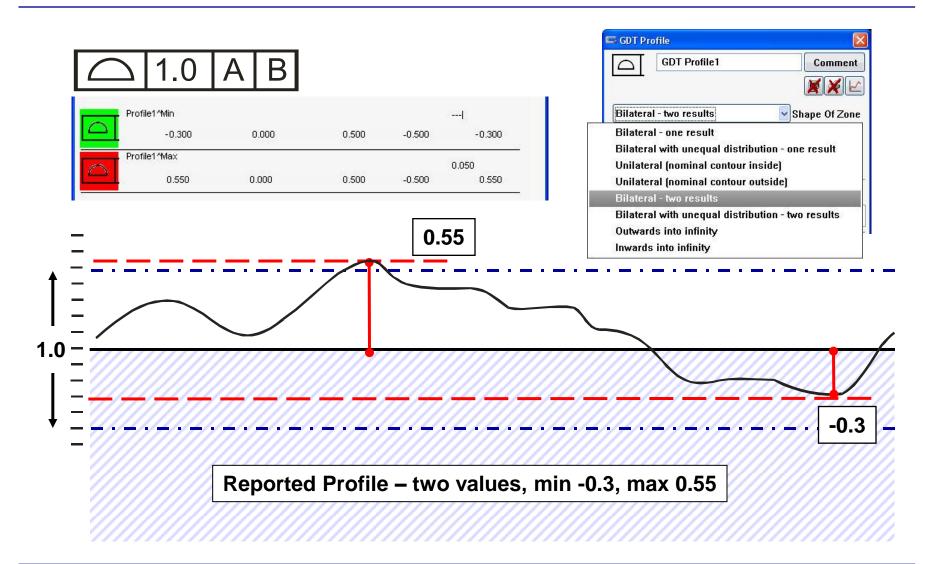


#### **Bilateral – one result** Double the largest deviation (inside and outside)



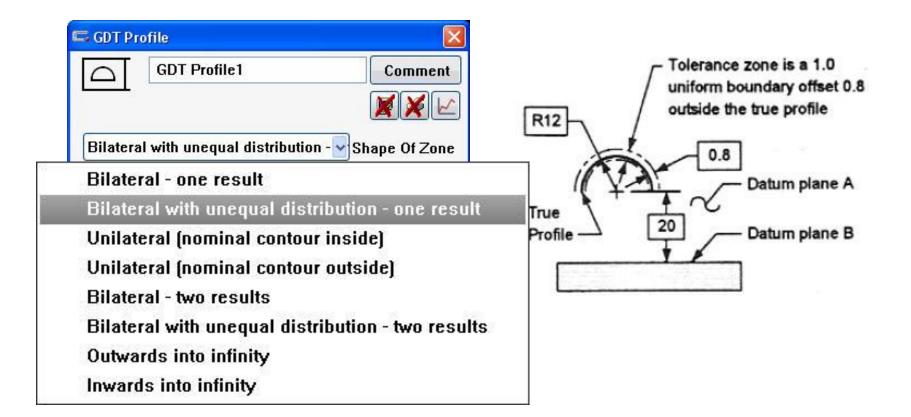
# Bilateral – two results (5.2)

#### The largest deviation inside and the largest deviation outside the workpiece.



#### Bilateral - (unequal distribution) - one result

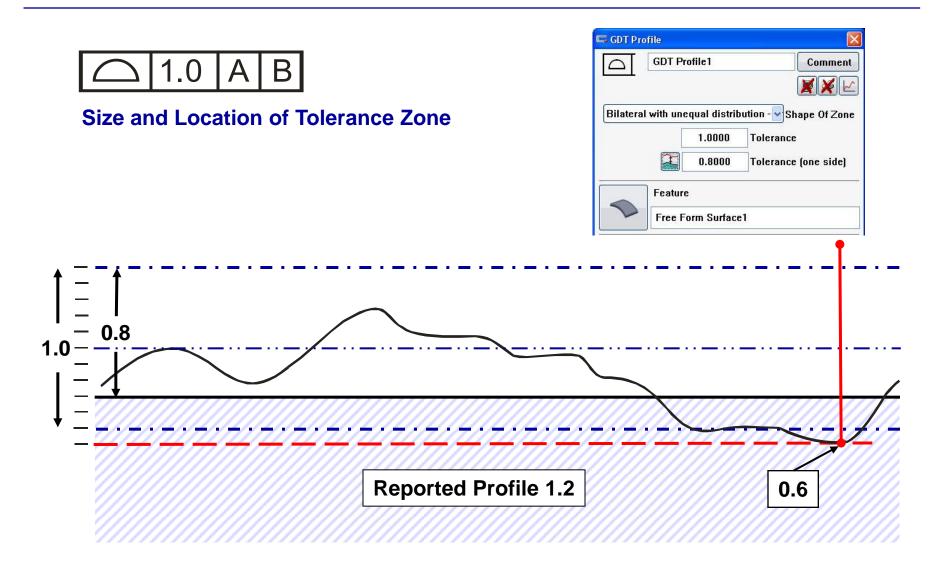
Double the largest deviation (inside and outside) from the calculated theoretical center line



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#### Bilateral - (unequal distribution) - one result

Double the largest deviation (inside and outside) from the calculated theoretical center line

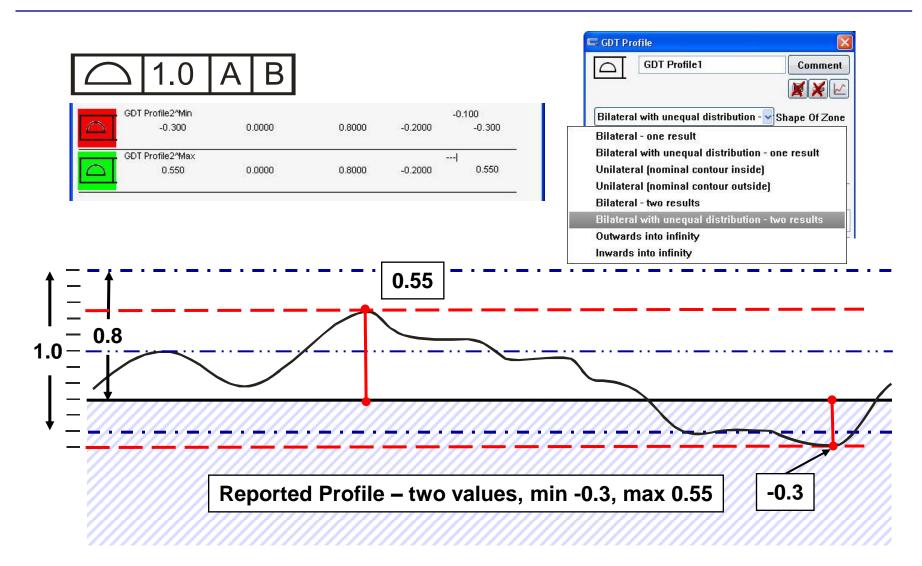


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#### Bilateral - (unequal distribution) – two results (5.2)









#### Bilateral – two results (5.2) The largest deviation inside and the largest deviation outside the workpiece.

Pr	ofile1^Min						
	-0.300	0.000	0.500	-0.500	-0.300		
Pr	ofile1^Max				0.050		
	0.550	0.000	0.500	-0.500	0.550		

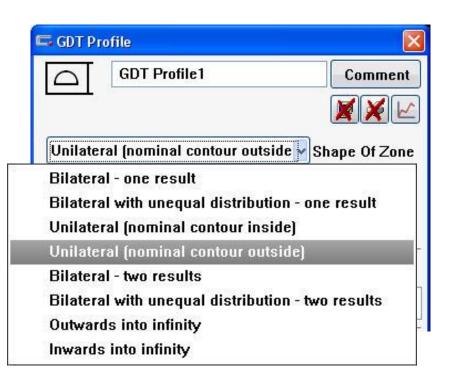
#### Bilateral - (unequal distribution) – two results (5.2)

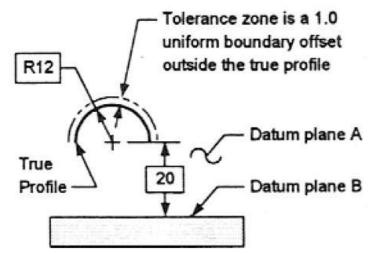
The largest deviation inside and the largest deviation outside the workpiece.

8636	GDT Profile2^Min		-0.100		
$\bigcirc$	-0.300	0.0000	0.8000	-0.2000	-0.300
	GDT Profile2^Max				-1
$\cap$	0.550	0.0000	0.8000	-0.2000	0.550

#### **Unilateral (nominal contour outside)**

Double the largest deviation from the tolerance average to the inside or outside

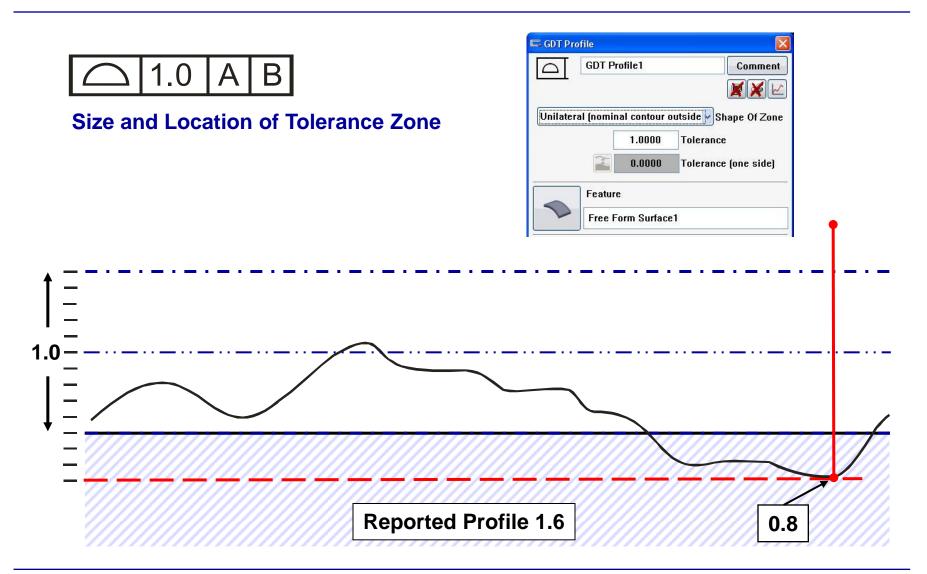




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#### **Unilateral (nominal contour outside)**

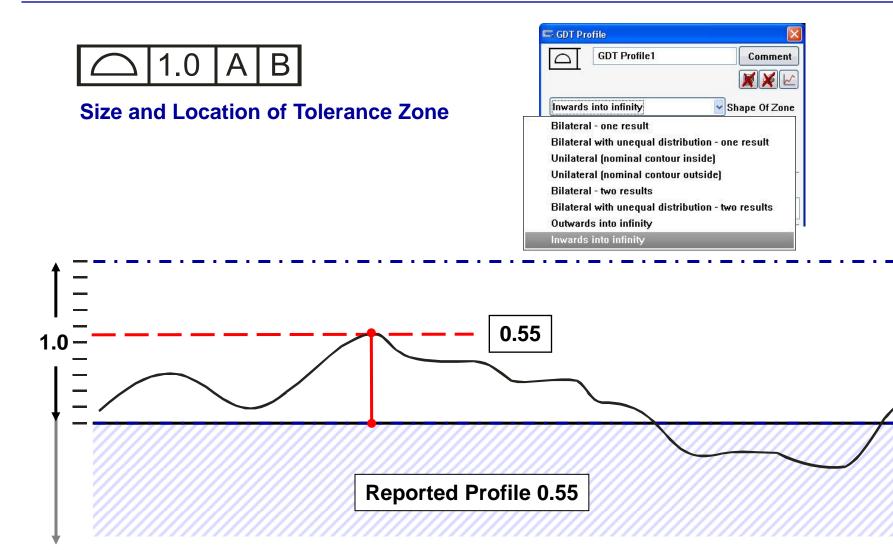
Double the largest deviation from the tolerance average to the inside or outside



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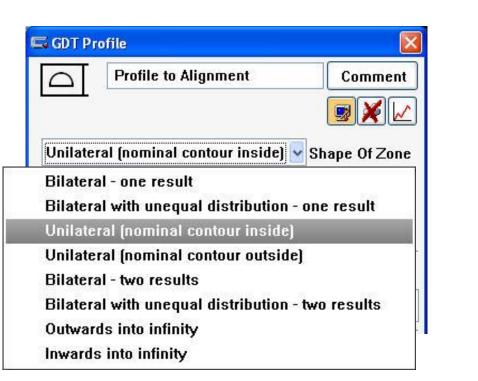
#### **Inwards into infinity** The largest deviation <u>outside</u> the workpiece

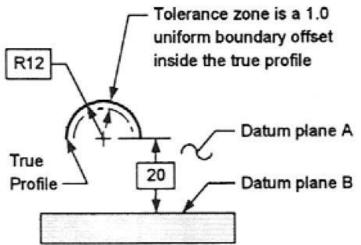




## **Unilateral (nominal contour inside)**

Double the largest deviation from the tolerance average to the inside or outside

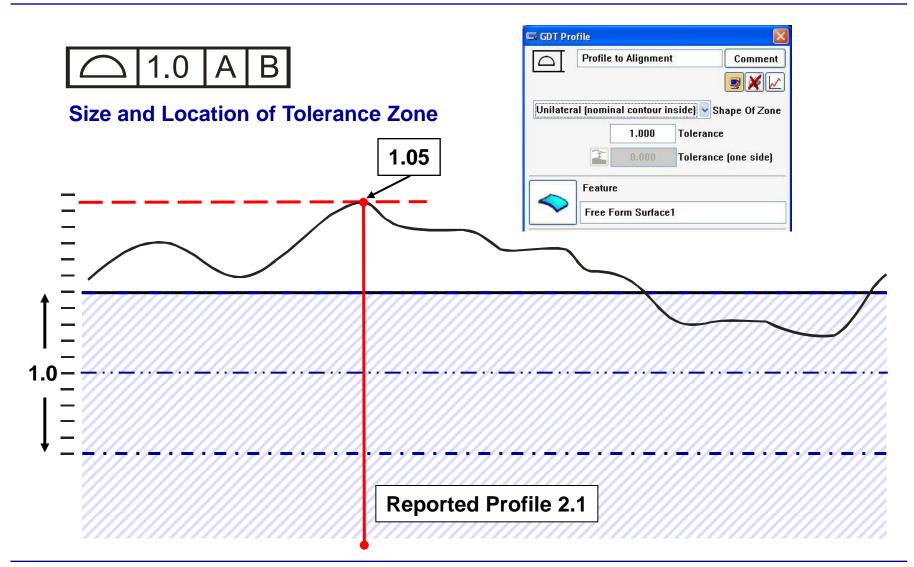






## **Unilateral (nominal contour inside)**

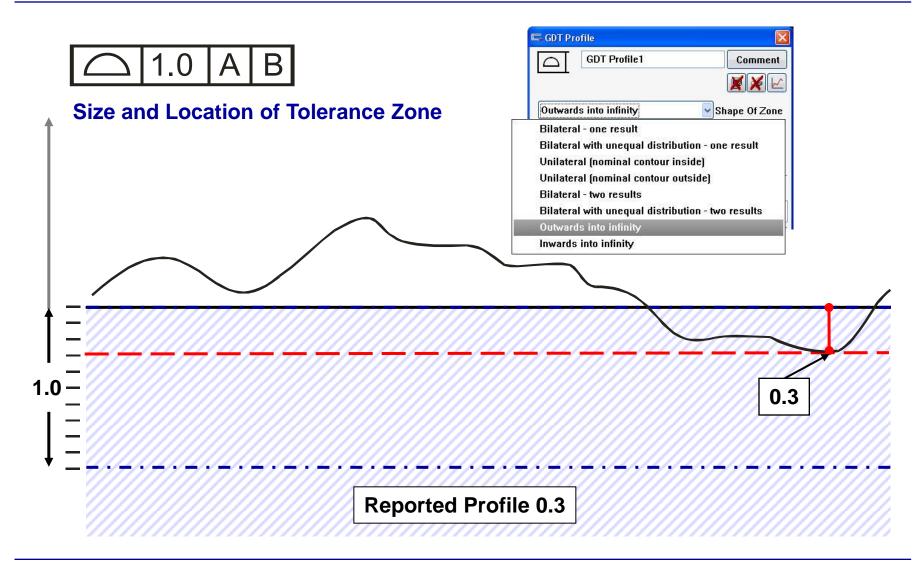
Double the largest deviation from the tolerance average to the inside or outside





#### Outwards into infinity The largest deviation <u>inside</u> the workpiece







# CALYPSO.

Calypso 4.10 - 5.2 mbusha 2009 - 2011